# **Alternative Approaches to Teaching Extended Surface Heat Transfer**

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## Introduction

Extended surface heat transfer is a topic that is always covered in a standard undergraduate class in heat transfer. In fact, we tell our students that fins are one of the two heat transfer systems that they will most likely encounter as practicing mechanical engineers (the other being heat exchangers). Therefore, it becomes clear that the mechanical engineering student needs to have a firm foundation in the physical aspects of extended surface heat transfer, and an understanding of the mathematical models available for the required calculations.

Two tools have been developed to facilitate the students' learning in these directions. The first tool consists of a set of physical models of the different types of fins. This allows the students to get a "hands-on" feel for fins. It is particularly useful for students whose primary learning style is kinesthetic. The second tool is an excel spreadsheet that calculates the standard fin parameters and presents the temperature distribution for a variety of fins using the three standard boundary conditions at the fin tip: adiabatic, convective, and tip at fluid temperature. A calculation option that is available to the user will determine the number of fins in an array that is required to provide a specified heat transfer rate requirement (may be heating or cooling). This option allows the students to perform some simple design studies and compare the performance of different fin types (for example rectangular versus triangular) and arrangements, including the tradeoffs in length, thickness, and orientation. For visual learners, the spreadsheet also includes a photograph of the physical model and a diagram relating the geometric parameters for each type of fin geometry.

These tools have been used in heat transfer classes at both Olivet Nazarene University and Michigan State University. At Olivet Nazarene the spreadsheet was used as a virtual design lab activity, while at Michigan State the spreadsheet was used as an extended homework assignment.

This paper continues with the development of the physical models. The corresponding mathematical models and the Excel spreadsheet are then presented. Next, the assignments for both classes are discussed along with results of student surveys on the tools and assignments. Final remarks conclude the paper.

## **Physical Background and Models**

Fins are used to enhance the heat transfer to or from a surface by increasing the surface area. To introduce this idea to students, the following scenario is proposed to them. Consider a computer circuit board that contains electronic components producing heat through I<sup>2</sup>R heating. To ensure proper operation and eliminate short lifetimes, the board must be maintained at a specified

temperature,  $T_{max}$ . A cooling system has been designed for this application which involves blowing air past the board to achieve convective cooling or

$$q = h_c A (T_{max} - T_{air})$$

where q will be equal to the electrical power dissipation. Of course, one of the things that is true about computers is that the customer always wants the machine to go faster and be more powerful. To achieve this a company might put even more electronic components on the board, which would lead to more electrical power dissipation, and if not addressed this would likely overheat the circuit board. So to maintain the new circuit board at the maximum operating temperature the cooling system must be redesigned. To gather a sense of what we might want to do let us look at our Newton's law of cooling.

$$q = h_c A (T_{board} - T_{air})$$

So if q is fixed, the students are asked what might be done to lower  $T_{board}$ . Three possible design alternatives are:

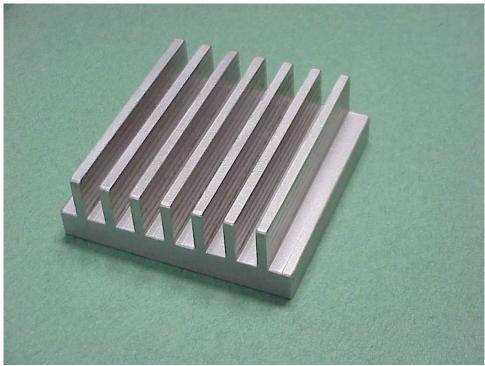
- increase h<sub>c</sub> increase air velocity or change to another fluid
- decrease T<sub>air</sub> refrigerate the air
- increase A add extended surfaces or fins to the circuit board

The addition of fins is argued to the students as being the simplest and probably most effective design alternative. It needs to be pointed out to the students that there are two major downsides to adding fins:

- (i) may negatively affect the flow of air around the circuit board and hence h<sub>c</sub>
- (ii) because of conduction the fin cannot be entirely at  $T_{\text{board}}$

At this point it proves useful to discuss the various types of fins. Physical models of four different fin types are available to pass around the classroom, so that the students may get a "feel" for what a fin array consists of. These physical models are shown in Figure 1. They were constructed by one of the authors (Ryan Harrier) as an undergraduate at Michigan State University. Detailed drawings and fabrication details may be obtained from the lead author at somerton@egr.msu.edu. Our experience has been that use of these props creates a much stronger understanding about the physical nature of fins than the pictures in a typical heat transfer text book. One of the authors has used some junked heat sinks from a computer shop that might be available from computer services on most campuses. Though not as simple and direct as the models made to match the textbook formulas, they still provide a hands-on experience for the students.

Figure 1 Pictures of Physical Models



Rectangular Fin Array



Cylindrical Fin Array

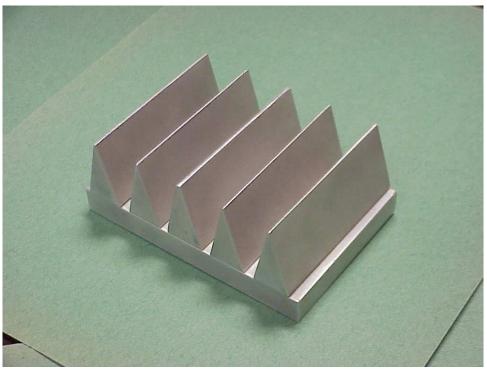


Figure 1 Pictures of Physical Models (continued)

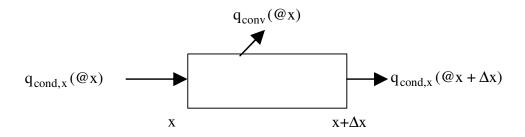
Triangular Fin Array



Annular Fin Array

#### Mathematical Background and Excel Workbook

The primary mathematical model for fins consists of the differential energy equation for the fin. The following derivation is used in our classes, and for completeness is included here. We consider the fin shown in Fig. 2. Then we consider a differential element  $\Delta x$  of this fin of arbitrary geometry and varying cross-sectional area, as shown below.



Performing an energy balance on this element yields

 $q_{\text{cond},x}(@x) = q_{\text{cond},x}(@x + \Delta x) + q_{\text{conv}}(@x)$ 

To make this useful we now need to use our constitutive equations to relate the heat flows to temperature. Then we have

$$\left. + kA_{c}(x)\frac{\partial T}{\partial x} \right|_{at x} = -kA_{c}(x + \Delta x)\frac{\partial T}{\partial x} \Big|_{at x + \Delta x} + h_{c}\Delta A_{s}(T(x) - T_{f})$$

The differential surface area in general can be given by

$$\Delta A_s = P(x)\Delta x$$

where P(x) is the perimeter of the fin. Substituting

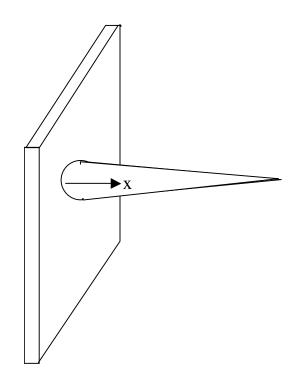
$$\left. + kA_{c}(x)\frac{\partial T}{\partial x} \right|_{at x} = -kA_{c}(x + \Delta x)\frac{\partial T}{\partial x} \Big|_{at x + \Delta x} + h_{c}P(x)\Delta x (T(x) - T_{f})$$

Now dividing through by  $k\Delta x$  and rearranging

$$\frac{A_{c}(x + \Delta x)\frac{\partial T}{\partial x}\Big|_{at x + \Delta x} - A_{c}(x)\frac{\partial T}{\partial x}\Big|_{at x}}{\Delta x} = \frac{h_{c}P(x)}{k} (T(x) - T_{f})$$

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and taking the limit as  $\Delta x \Rightarrow 0$  and using the definition of the derivative

$$\frac{\mathrm{d}}{\mathrm{d}x}\left(\mathrm{A}_{\mathrm{c}}(\mathrm{x})\frac{\mathrm{d}\mathrm{T}}{\mathrm{d}x}\right) - \frac{\mathrm{h}_{\mathrm{c}}\mathrm{P}(\mathrm{x})}{\mathrm{k}}\left(\mathrm{T}(\mathrm{x}) - \mathrm{T}_{\mathrm{f}}\right) = 0$$

This second order, variable coefficient, non-homogeneous differential equation is the most general form of the energy equation for heat transfer through a fin. Though various geometries could now be considered and the differential equation solved, a typical heat transfer class only has time to develop the mathematical solution for the case of a fin of constant cross-sectional area. For this case the differential equation simplifies to

$$\frac{\mathrm{d}^2\theta}{\mathrm{d}x^2} - \mathrm{m}^2\theta = 0$$

where

$$m = \sqrt{\frac{h_c P}{k A_c}}$$

and we have defined an excess temperature,  $\theta$ ,

$$\theta = T(x) - T_{\rm f}$$

The general solution will take the form

 $\theta = D_1 \cosh(mx) + D_2 \sinh(mx)$ 

where the constants  $D_1$  and  $D_2$  will be evaluated from the boundary conditions. At the base of the fin, x = 0, we typically assume a known temperature, or

at 
$$x = 0$$
,  $T(0) = T_{base}$  or  $\theta(0) = T_b - T_f$ 

At the tip of the fin we may have any of the three standard thermal boundary conditions. If the fin is long enough, we might suppose that it would reach the surrounding fluid temperature at the tip

at x = L,  $T(L) = T_f$  or  $\theta(L) = T_f$ - $T_f = 0$ 

Again if the fin is long enough, we might argue that all of the heat will leave by the sides before it gets to the tip, so that the tip would be adiabatic (have zero heat flow). Then our boundary condition would be

at x = L, 
$$-k \frac{dT}{dx}\Big|_{x=L} = 0$$
 or  $\frac{d\theta}{dx}\Big|_{x=L} = 0$ 

Finally, the most general boundary condition (not concerned with having a "long" fin) is the convective condition or

at x = L, 
$$-k \frac{dT}{dx}\Big|_{x=L} = h_{tip} [T(x = 0) - T_f]$$
 or  
 $\frac{d\theta}{dx}\Big|_{x=L} + \frac{h_{tip}}{k} \theta (x = L) = 0$ 

Note that the convective heat transfer coefficient at the tip as been denoted as a different variable  $(h_{tip})$  than the heat transfer coefficient acting on the side  $(h_c)$ . This will allow us to take the convective tip solution and obtain the other two cases by letting  $h_{tip}$  go to zero (the adiabatic tip case) or letting  $h_{tip}$  go to infinity (the tip at fluid temperature case).

Applying the general convective tip boundary condition gives the following expression for the excess temperature

$$\theta = \theta_{b} \cosh(mx) - \frac{\theta_{b} \left[ \frac{h_{tip}}{k} + m \cdot tanh(mL) \right]}{m + \frac{h_{tip}}{k} tanh(mL)} sinh(mx)$$

From this expression and the standard definitions the fin heat transfer rate, fin thermal resistance, and fin efficiency can all be obtained as shown below.

$$q_{fin} = \frac{\sqrt{hPkA_c}\theta_b \left[\frac{h_{tip}}{m \cdot k} + tanh(mL)\right]}{1 + \frac{h_{tip}}{m \cdot k}tanh(mL)}$$
$$R_{fin} = \frac{1 + \frac{h_{tip}}{m \cdot k}tanh(mL)}{k \cdot m \cdot A_c \left[\frac{h_{tip}}{m \cdot k} + tanh(mL)\right]}$$

$$\eta_{\text{fin}} = \frac{\sqrt{hPkA_c} \left[ \frac{h_{\text{tip}}}{m \cdot k} + \tanh(mL) \right]}{hA_{\text{s,fin}} \left[ 1 + \frac{h_{\text{tip}}}{m \cdot k} \tanh(mL) \right]}$$

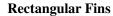
The Excel spreadsheet FinSolver.xls has been developed using these expressions. The workbook is composed of five spreadsheets, each for a different fin geometry. As indicated by the worksheet tabs, calculations may be made for rectangular fins, cylindrical fins, triangular fins, annular fins, or parabolic fins. Each worksheet has a similar layout, so for demonstration purposes, we consider the rectangular fin spreadsheet. The spreadsheet is divided into three parts. Fig. 3 shows part 1 of the rectangular fin spreadsheet. At the top is a drawing that labels the pertinent dimensions of the fin and a picture of the physical model of a rectangular fin array. Beneath these pictures, cells are provided for the required inputs for the fin analysis. As shown in Fig. 4, part 2 of the spreadsheet provides the results of the fin analysis for the inputs specified. This includes the temperature, heat transfer rate, efficiency, and thermal resistance for the three different boundary condition cases discussed above. The temperature distribution is provided graphically for the three cases, so students can clearly see the differences or similarities among the solutions as input parameters are varied. The third and final part of the spreadsheet (see Fig. 5) has been set up to allow students to explore some design issues associated with fin arrays. The student will specify the heat transfer required and the base surface area available, and the spreadsheet will calculate the number of fins and their mass per the inputs provided in part 1 to fulfill the requirements. The spreadsheet may be downloaded from the web at

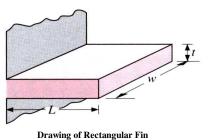
#### http://www.msu.edu/~somerton/Fins

#### Assignments and Student Feedback

At Olivet Nazarene University FinSolver.xls was used in a virtual design lab activity for the junior-senior level heat transfer course, ENGN 385. The assignment and a suggested procedure are shown in Figs. 6 and 7. At Michigan State University FinSolver.xls was used in an extended homework assignment for the senior level heat transfer course, ME 410, and is shown in Fig. 8. For the ME 410 assignment, one lecture period was taken to introduce the students to FinSolver.xls using a computer projection system. For ENGN 385, the instructor spent about thirty minutes in the lab with students logged in on computers, so as to have the spreadsheet available in front of them, while the instructor, using a computer projection system, demonstrated features of the program and worked out a first trial case of the assignment. The clear difference in the nature of these two assignments shows the utility of the spreadsheet.

## Figure 3 Part 1 of Rectangular Fin Spreadsheet







Picture of Rectangular Fin Array

				Inputs					
Width (m)	Length (m)	Thickness (m)	Heat Transfer Coefficient (W/m <sup>2</sup> ·K)	Base Temperature (°C)	Fluid Temperature (°C)	Thermal Conductivity (W/m·K)	Density (kg/m <sup>3</sup> )	Tip Heat Transfer Coefficient (W/m <sup>2</sup> ·K)	Distance at which temperature is desired (m)
0.36	0.05	1.00E-03	23	250	33	21.9	4500	100	0.05

#### Figure 4 Part 2 of Rectangular Fin Spreadsheet

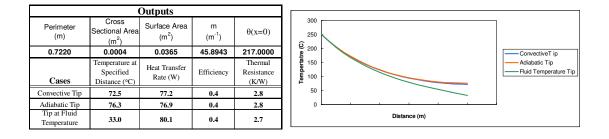


Figure 5 Part 3 of Rectangular Fin Spreadsheet

Design Analysis					
Input	Input	Output	Output		
Required Heat Transfer (W)	Bare Surface Area (m <sup>2</sup> )	Number of Fins	Mass of Fin Array (kg)		
300	0.13	4	0.324		

Tiger Engineering

TO:Thermal Design TeamFROM:Product DevelopmentDate:March 14, 2002

Due: Thursday, April 4, 2002.

The Product Development Team has produced a novel conceptual design that will display realtime stock quotes, basketball scores, and Krispy-Kreme delivery times in high-intensity purple and gold, using data downloaded from a wireless network. However, the sensitive electronics inside require that the housing temperature be maintained at or below 30 °C. The device has a peak power consumption rate of 25 W.

We require you to investigate possible finned heat-sink designs using aluminum, copper, and stainless steel. We are seeking the most cost-effective feasible design, since it is hoped that demand for the device will drive mass-production quantities.

Please document your design recommendations, and also your analyses of those designs considered, in a technical report so that designers for future products can build upon your work. Document assumptions made and any additional considerations which may be needed for design refinement or future product designs.

In addition, please determine the sensitivity of your design to the convective coefficient, h. The given value is a design estimate based on the flow enhancement available from the small fan.

Also be prepared to request improvements in the Fin Solver tool from the Technical Computing Department that would better facilitate these analyses.

You should base your analysis on the standardized design data that accompanies this memo.

Please submit your technical report by Thursday, April 4, 2002.

Design Data	
Product	
Power dissipation	q = 25  W
max. allowable surface temperature	$T_{s,max} = 30 ^{\circ}\mathrm{C}$
surface available for heat sink	$8.5 \text{ cm} \times 15 \text{ cm}$
aluminum	
unit cost	$D_{Al} = $13.77 \text{ /kg}$
density	$\rho_{Al} = 2770 \text{ kg/m}^3$
conductivity	$k_{Al} = 177 \text{ W/m} \cdot \text{K}$
copper	
unit cost	$D_{Cu} = \$9.15 / \text{kg}$
density	$\rho_{Cu} = 8850 \text{ kg/m}^3$
conductivity	$k_{Cu} = 390 \text{ W/m} \cdot \text{K}$
stainless steel	
unit cost	$D_{SS} = \$8.66 / \text{kg}$
density	$\rho_{SS} = 8055 \text{ kg/m}^3$
conductivity	$k_{SS} = 15.1 \text{ W/m} \cdot \text{K}$
Environment	
ambient temperature	$T_{\infty} = 22 ^{\circ}\mathrm{C}$
avg design convection coeff	$h = 25 \text{ W/m}^2 \cdot \text{K}$

# Figure 6 Virtual Design Lab Assignment (continued)

Figure 7 Procedure for Virtual Design Lab Assignment

## ENGN 385 Spring 2002 Suggested Procedure for Fin Design Lab

- 1. Copy the **Fin Solver.xls** spreadsheet from the 385 directory of the O: drive.
- 2. To start, choose one material (say, Aluminum) and one geometry (say, rectangular fins).
- 3. Enter the design parameters for input.
- 4. Begin with a "reasonable" design choice for one parameter (say, the length).
- 5. Determine the other design criteria (thickness of each fin) that satisfy the design problem requirements. Verify that the number of fins required is reasonable (that they will fit onto the surface with a reasonable spacing!)
- 6. You now have one **feasible design**, meaning one that is physically achievable (realistic) and that fits the bill on the design requirements.
- 7. Determine the weight and cost for this design. (You may want to add this calculation to your spreadsheet.)
- 8. Vary the length parameter chosen in step 3, and determine additional **feasible designs**. Determine the weight and cost for these designs.
- 9. As you begin to gain an understanding of the relationship between the parameters, you may want to use the *Goal Seek* and/or the *Solver* tools in Excel to quickly identify each feasible design, and even to optimize the design to minimize weight and cost.
- 10. Perform similar analyses with the other possible materials and fin geometries (rectangular, cylindrical pins, triangular, and parabolic).

#### Figure 8 Extended Homework Assignment

# ME 410 Fin Analysis Using FinSolver.xls

For problems 1-3 consider a rectangular fin of width 15 cm and thickness 0.05 cm composed of plain carbon steel. The base temperature is 100°C and the fluid temperature is 20°C.

- 1. For a side convective heat transfer coefficient of  $1 \text{ W/(m}^2 \text{ K})$  and a length of 10 cm, determine the tip convective heat transfer coefficient that will
  - (a) have the convective tip solution behave like the adiabatic tip solution
  - (b) have the convective tip solution behave like the tip at fluid temperature solution
- 2. For the side and tip heat transfer coefficient equal to each other, determine the conditions (length and convective heat transfer coefficient) that will
  - (a) have the convective tip solution behave like the adiabatic tip solution
  - (b) have the convective tip solution behave like the tip at fluid temperature solution
- 3. Starting with a fin of length 10 cm and a convective heat transfer coefficient of 40 W/( $m^2$  K), determine how the fin efficiency varies with
  - (a) thermal conductivity
  - (b) fin length
  - (c) fin thickness
  - (d) fluid temperature
  - (e) convective heat transfer coefficient
  - (f) fin width
- 4. From the analyses performed above, evaluate how good of an approximation is the adiabatic tip model for a real fin (convective tip model).
- 5. A surface of area 0.13 m<sup>2</sup> has a heat flow of 300 W and a temperature of 250°C. For rectangular fin of 0.36 m wide, 0.05 m long, made of titanium, determine the fin thickness that will minimize the mass (and hence cost) of the fin array. The convective heat transfer coefficient may be taken to be 23 W/(m<sup>2</sup> K) and the fluid temperature is at 33°C.
- 6. Repeat problem 5 for a triangular fin array.
- 7. Comparing the results of problems 5 and 6, which fin geometry will cost less for this application.

Student feedback on the use of FinSolver.xls and the assignments were obtained via the survey form shown in Fig. 9. Results of these surveys are shown separately for MSU and Olivet-Nazarene in Fig. 10. It is striking to note that the student's assessment of how the assignments improved their understanding of fins was significant, as the average response from question 1a to question 1b went from 2.9 and 2.6 to 4.2 and 4.1. This increase in understanding is further supported by the students written comments:

"The project helped me to visualize the concepts of extended surfaces. I understood how to do fin problems, but now I have more than just a theoretical understanding."

"The ability to see the results graphically helped make the concepts sink in."

"This software helps to try different situations so it's easier to understand the behavior of the fins."

There is also a significant difference between the MSU response (3.7) and Olivet-Nazarene response (2.9) to question 2a, but this is due to the difference in the nature of the two assignments. The extended homework assignment made to the MSU students was clearly more focused on the heat transfer principles than the design assignment for the Olivet-Nazarene students. Another significant difference exists between the two cohort groups for question 5. This is probably due to the fact that the Olivet-Nazarene students were asked to use the Solver function Excel, and it is our experience that most students have little experience with this function. Finally, all students felt that they needed more direction on the assignments, but out experience is that students, in general, are very uncomfortable with these types of open ended assignments. The written comments were very supportive of the spreadsheet program, though several urged that a tutorial and a drop-down material database should be developed.

#### **Final Remarks**

A spreadsheet program, FinSolver.xls, has been used in heat transfer classes at both Michigan State University and Olivet-Nazarene University. Student feedback indicates that the assignments using the spreadsheet significantly improve the students understanding of fins. Based on the responses of students, a tutorial is being developed that will provide the students with additional direction in the use of the program.

## Fin Project **Student Assessment Survey**

		Did not understand = (0) Understood well = (5)
1.	Rate your understanding of fins	
	a) before starting this project and	0 1 2 3 4 5
	b) after completing this project	012345

## COMMENTS:

		Did not understand = (0) Understood well = (5)
2.	How well did this project improve your understanding	
	of	
	a) the heat transfer principles of fins	0 1 2 3 4 5
	b) the analysis of fins	0 1 2 3 4 5
	c) the design of fins	0 1 2 3 4 5
	d) the use of a spreadsheet as a design tool	0 1 2 3 4 5

#### COMMENTS:

	Did Not help= $(0)$
	Enhanced very much $= (5)$
•	

Did the ability to use the program to explore the effect 3. of several parameters on fin performance enhance your learning about fins?

0 1 2 3 4 5

#### **COMMENTS:**

Figure 9 Student Survey (continued)

		Strongly disagree = $(0)$
		Strongly Agree $= (5)$
4.	I knew what I was expected to do for this project.	0 1 2 3 4 5

- COMMENTS:
- 5. I had the knowledge and tools to effectively complete ① ① ② ③ ④ ⑤ this project.

COMMENTS:

6. What would you suggest to improve this project?

7. What would you suggest to improve the fin solver program?

8. Give this assignment a grade A - F.

	Averages	
Questions	MSU	Olivet- Nazarene
1a) Rate your understanding of fins		
before starting this project	2.9	2.6
1b) Rate your understanding of fins		
after completing this project	4.2	4.1
2a) How well did this project		
improve your understanding of the		
heat transfer principles of fins	3.7	2.9
2b) How well did this project		
improve your understanding of the		
analysis of fins	3.8	3.4
2c) How well did this project		
improve your understanding of the		
design of fins	4.1	4
2d) How well did this project		
improve your understanding of the		
use of a spreadsheet as a design tool	4.1	4
3) Did the ability to use the program		
to explore the effect of several		
parameters on fin performance		
enhance your learning about fins?	4.0	4
4) I knew what I was expected to do		
for this project	3.1	3.1
5) I had the knowledge and tools to		
effectively complete this project	4.2	3.1
Give this assignment a grade A – F	3.22	3.13

Figure 10 Survey Results

#### CRAIG W. SOMERTON

Craig W. Somerton is an Associate Professor and Associate Department Chair of Mechanical Engineering at Michigan State University. He teaches in the area of thermal engineering including thermodynamics, heat transfer, and thermal design. Dr. Somerton has research interests in computer design of thermal systems, transport phenomena in porous media, and application of continuous quality improvement principles to engineering education. He received his B.S. in 1976, his M.S. in 1979, and his Ph.D. in 1982, all in engineering from UCLA.

#### JOSEPH BAYNE SCHROEDER

Joseph is Associate Professor of Engineering at Olivet Nazarene University, where he teaches mechanical engineering and physics courses. Joseph earned a B.S.M.E. from the University of Illinois at Urbana-Champaign in 1991, an M.S. in mechanical engineering from Michigan State University in 1994, and is a Ph.D. candidate in mechanical engineering at MSU, with research in computational analysis of flow in porous media. His interests include effective active and collaborative learning methods, design optimization, parameter estimation, and thermal system design.